

# Modeling and Optimisation of Hybrid Solar Water Desalination System in Indonesia

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## Abstract

Clean water demand has significantly increased due to the rise in the global population. Only 2.5% of the total water source on the Earth is freshwater, while the remaining water has high saline content that cannot be consumed directly. Desalinated water is one of the potential solutions to meet the growing demand for freshwater, which is highly energy intensive. This paper analyses the energy, economic and environmental performance of a 5 m<sup>3</sup> PV (photovoltaic) powered reverse osmosis (RO) desalination system. Three scenarios of PV-RO with and without battery storage and diesel generator hybrid systems have been analyzed and investigated for the annual estimate load, net present value, and payback period of the water and electricity production costs. Concurrently, the CO<sub>2</sub> avoidance over the lifetime operation of the designed PV-RO desalination plant is evaluated. In this study, the analysis shows that the PV-RO system without battery 6.3 kW PV panels installed with a 2-days water storage tank system is optimized and economically feasible. The Levelized Cost of Electricity (LCOE), Levelized Cost of Water (LCOW), and Payback Period (PBP) are found to be \$0.154/kWh, \$0.627/m<sup>3</sup>, and five years, respectively. The CO<sub>2</sub> emissions avoidance by the PV-RO system without a battery was 65,152.5 kg.CO<sub>2</sub>eq, while the optimized system could eliminate 111,690 kg.CO<sub>2</sub>eq per year.

**Keywords:** Desalination, Photovoltaic, Reverse osmosis, Solar energy, Hybrid power system.

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## 27 Symbols and Abbreviations

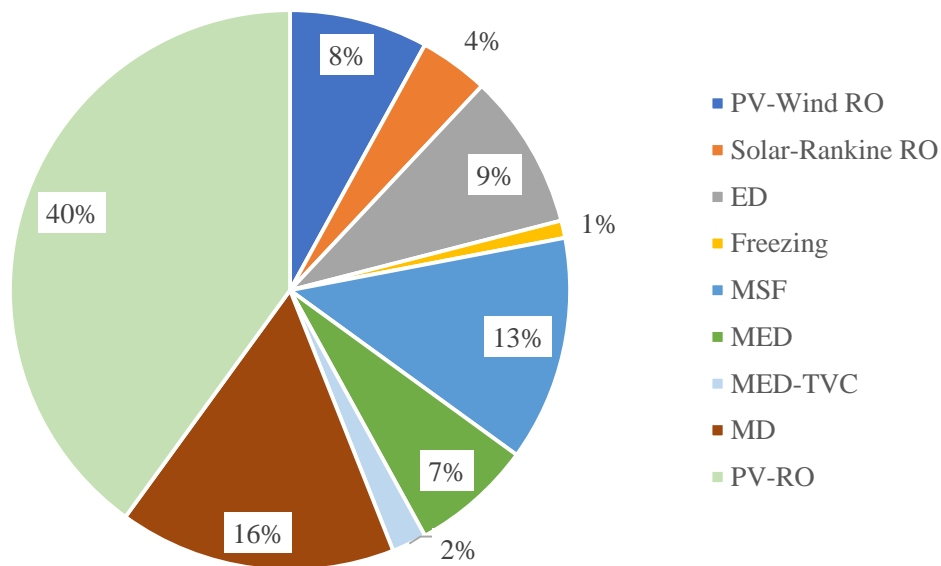
<b>Symbols</b>	<b>Unit</b>	<b>Description</b>
TDS	ppm	Total Dissolved Solids
$E_{load}$	kWh	Daily energy required
$E_{system}$	kWh/m <sup>3</sup>	The energy required per cubic meter of water production
$I_{loss}$	kWh	Inverter loss
$Au_{loss}$	kWh	Auxiliary loss
$E_{tot}$	kWh	Daily load profile calculated for the system
$\eta_{BOS}$	%	Balance of system efficiency
$E_p$	kWh	The energy produced by a panel
$A$	m <sup>2</sup>	Solar panel area
$H$	kWh/m <sup>2</sup> /day	Average solar radiation
$PV_{req}$	-	Number of panels required
$\eta_p$	%	Efficiency of panel
$F_0$	L/hr/kW	Fuel curve intercept coefficient
$F_1$	L/hr/kW	Fuel curve slope
$Y_{gen}$	kW	Rated capacity of the generator
$P_{gen}$	kW	The electrical output of the generator
$DoD$	%	Battery depth of discharge
$\eta_b$	%	Efficiency of battery
$CF$	\$	Annual Cash Flow
MARR	%	Minimum Attractive Rate of Return
LCOE	\$/kWh	Levelized Cost of Electricity
LCOW	\$/m <sup>3</sup>	Levelized Cost of Water
PBP	year	Payback Period
IRR	%	Internal Rate of Return
NPV	\$	Net Present Value
CAPEX	\$	Capital Expenditures
OPEX	\$	Operating Expenditures
COD	-	The chemical oxygen demand
BOD	-	The biochemical oxygen demand
MED	-	Multiple-effect distillation
MSF	-	Multi-stage flash
RO	-	Reverse osmosis

## 29 **1. Introduction**

30 Water and energy are the essences of modern human needs. The development of any nation is highly  
31 dependent on the availability of clean water and energy. The energy is needed to produce and supply  
32 the water, so the energy demand is accelerated with the increasing demand for clean water. Like  
33 many countries, clean water scarcity is also a severe problem in Indonesia. Only 47.71% of the total  
34 population in Indonesia has proper access to clean water sources [1]. About 70% of water usage is  
35 used for agricultural purposes, with 9% for industry and 11% for domestic activities [2]. However,  
36 fossil-based energy generation, which is still the main energy source for water production and supply,  
37 has sparked global warming and climate changes. Therefore, producing clean water from the  
38 renewable energy assisted desalination process can address the water shortage challenges and reduce  
39 climate changes. There are 16,876 desalination plants operated globally, with 85% using the RO  
40 system, 270 plants under construction, and 3,825 offline plants [3]. The combination of a desalination  
41 system and renewable energy is not new and has already been implemented worldwide. Most of  
42 these renewable energy based desalination plants are driven by solar energy. Note that the solar water  
43 desalination separates salt from saline water to obtain clean water using solar energy as the power  
44 source. **Figure 1** shows the percentage of the global renewable energy based desalination plant. The  
45 solar-powered plant occupies nearly half of the total, followed by wind and geothermal.

46 The desalination technology can be differentiated into two types; thermal technologies such as  
47 multiple-effect distillation (MED) or multi-stage flash (MSF) and membrane processes, including  
48 reverse osmosis (RO). Thermal processes generally come with a higher capital cost and are  
49 noticeably energy intensive. On the other hand, RO technology has a lower capital cost but higher  
50 maintenance spending and is unsuitable for high salinity or poor water quality. The RO process is  
51 also easy to upgrade and requires around 25% less area than the MED. The membrane plays the most  
52 vital role in the RO process without heating or phase change. The RO membranes have a dense  
53 barrier layer which is selective for not allowing large molecules or ions through its pores but allows  
54 solvent to pass through the thick layer freely. High pressure is required for conducting the RO

55 process, usually 2-17 bar (30-250 psi) for brackish water and 40-70 bar (600-1000 psi) for seawater  
 56 [4]. Generally, the RO process consumes about 3.5 kWh/m<sup>3</sup> of energy for brackish water (Kaya et  
 57 al., 2019) and approximately 6.99 kWh/m<sup>3</sup> for seawater [5]. The variation of solar energy outputs of  
 58 heat or electricity lead to further considerations in designing a desalination system. In Indonesia, the  
 59 combination of solar photovoltaics and reverse osmosis (PV-RO) has a high potential to be  
 60 implemented. The primary energy requirement in RO is for pressurizing the feed water.



61  
 62 **Figure 1.** Desalination technologies are powered by solar energy [6]

63 PV technology is ideal for powering RO units, particularly in remote areas where the electricity grid  
 64 is inaccessible [7]. It can either be used as a standalone or hybrid system with another energy source  
 65 such as batteries, wind, and diesel engines. As a renewable source for desalination, the wind turbine  
 66 has been used since the early 1980s [8]. Compared to the hybrid Diesel-PV-RO system in which the  
 67 energy generation is executed by PV and transfers to diesel if the energy generated does not meet  
 68 daily requirements, the PV-RO standalone system has a high capital cost but lower operating cost  
 69 than the hybrid Diesel-PV-RO system. A buffer tank is usually installed to increase the productivity  
 70 of the PV-RO system. This tank is used as the storage system for permeation in the range of 28% to  
 71 36% based on the pressure applied [9]. Another approach to increase productivity is by developing  
 72 high capacity dual-stage plant. A study showed that a dual-stage plant with a capacity of above 5 m<sup>3</sup>  
 73 could have a high recovery rate of 65%. In comparison, a desalination plant with a capacity below 5

74 m<sup>3</sup> was not economically feasible as increasing capacity will reduce the production costs [10]. On  
75 the other hand, the efficiency of PV systems has increased during the past decade through different  
76 methods, including solar tracking addition, tilt angle adjustment, autonomous cleaning systems, and  
77 cooling/preheating [11].

78 In terms of an economic view, the RO desalination process requires a relatively high capital cost,  
79 preventing its large-scale commercialization. The RO vessels consumed nearly one-third of the total  
80 cost, followed by seawater pre-treatment and electrical systems by 18.6% and 17.8%, respectively  
81 [12]. Thus, the initial stages of a desalination project need to be suitably forecasted for financial  
82 feasibility. This forecast includes the financing, permitting, operation and maintenance costs, and the  
83 environmental and social related expenses. Much of the cost component depends on the plant  
84 capacity, power generation, location, environmental conditions, feed water quality, and projected life  
85 span. The increase in feedwater's salt content would likely increase the operating costs as it requires  
86 more treatment and technologies. Generally, seawater as the feedwater to a desalination plant will  
87 probably cost five times more than brackish water as feedwater for a given size of the plant and water  
88 production. Also, more than half of the total costs of the desalination system are for thermal or  
89 electrical energy requirements to power pumps and other equipment. Thus, the PV-RO desalination  
90 plant offers exciting and affordable technology to provide clean water to the community. Also, PV-  
91 RO offers a competitive price at a lower capacity, unlike other technologies, which require large  
92 water treatment capacities to lower the cost per unit of clean water produced. Thus, leveraging  
93 financial measures for the distillation method has efficiently reduced freshwater costs.

94 Moreover, the environmental impact of a PV-RO desalination system would be low. Brine discharge  
95 from the desalination process is considered a significant environmental impact because it carries  
96 almost all the liquid waste. As a result, this waste affects most aquatic life, which is mainly credited  
97 to chemical components [13]. The impact of the temperature and pH of the brine is minimal as the  
98 temperature of the brine approaches the water input temperature with a maximum difference of about

99 2 °C in an RO system [14, 15]. In addition, renewable energy sources can reduce the possible  
100 greenhouse gas (GHG) emissions compared to that fossil energy sources.

101 The following specific problems have been identified in the present research work to address the  
102 opportunities and challenges of the PV-RO system in Indonesia:

- 103 • Clean water production in Indonesia is not sufficient for sustainable supply.
- 104 • A desalination system requires high energy, so finances are the primary issue.
- 105 • There is a low level of research based on technology enhancement and economic and  
106 environmental assessment of solar desalination for water production.

107 The overall objective of this study is to explore the potential of RO desalination with solar PV  
108 systems in Indonesia by evaluating the energy, economic and environmental impacts of the  
109 integrated renewable energy system. The proposed study investigates the performance of reverse  
110 osmosis desalination with solar energy generation by simulating different power generation  
111 scenarios. The scenarios utilize an integrated design concept for optimizing energy performance,  
112 costs, and environmental impact. The anticipated cost of production and maintenance is low since  
113 cheaper material could be used and result in significant CO<sub>2</sub> emission reduction to the environment.

## 114 **2. Methodology**

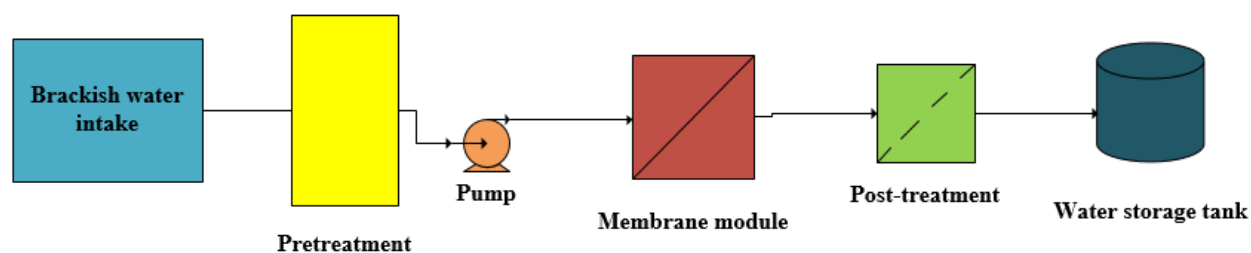
### 115 **2.1 Site description and input parameters**

116 The studied PV-RO system is assumed to be installed on Parang Island, part of Karimunjawa islands,  
117 Indonesia (5°49.2'S, 110°27.5'E). This selection is based on several factors: the lack of fresh water  
118 in some areas, high solar irradiance throughout the year, and lack of awareness of the health impacts  
119 of consuming brackish water from the inhabitants. Karimunjawa Islands is one of the exotic islands  
120 located in the Java Sea, specifically about 120 km north of Semarang, Java Island. The Parang  
121 island's population is approximately 10,000 inhabitants, primarily working as fishermen.

122 The island's topography is an undulating lowland with an altitude ranging from 0–506 meters above  
123 sea level with a total area of 71.2 km<sup>2</sup>. The maximum daily water requirement was estimated based  
124 on consumption of 3.3 liters per day per person. Therefore, the daily water capacity for the PV-RO  
125 system is 5 m<sup>3</sup> per day. The total dissolved solids (TDS) assumption used in the current study is  
126 32,000 mg/L [16].

## 127 2.2 The PV-RO Plant Design

128 A simplified flowsheet for the RO plant is shown in **Figure 2**. Pretreated brackish water flows to the  
129 pump with a pressure between 15 to 40 bars to be desalinated further. Permeate leaving the  
130 desalination system should have a level of TDS lower than 500 ppm to meet the drinking water  
131 criteria [17], and the reject is discharged into the discharge. Filmtec BW 2.5-inch membranes are  
132 used in the desalination process. Post-treatment includes the disinfection and mineralization process  
133 whereby the unused liquid goes to saltwater waste treatment and disposal.



134

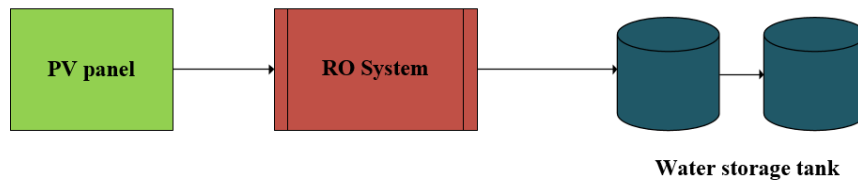
135 **Figure 2.** Process flow of RO desalination plant

136 This research defined three different power sources configuration to provide electricity to the  
137 desalination unit. A 5 m<sup>3</sup> storage tank will be installed in each scenario to store produced water. The  
138 specific energy consumption of the PV-RO system studied in this work was considered to be 3.5  
139 kWh/m<sup>3</sup>/day [18]. The project lifetime for the PV-RO desalination plant is 20 years.

### 140 2.2.1 Batteryless PV-RO System

141 The first scenario of the PV-RO system is installing a standalone PV system to power the desalination  
142 without battery storage. Because of this arrangement, the plant will only produce freshwater during  
143 sunshine hours daily. The details of this scenario are shown in **Figure 3**. This primary combination

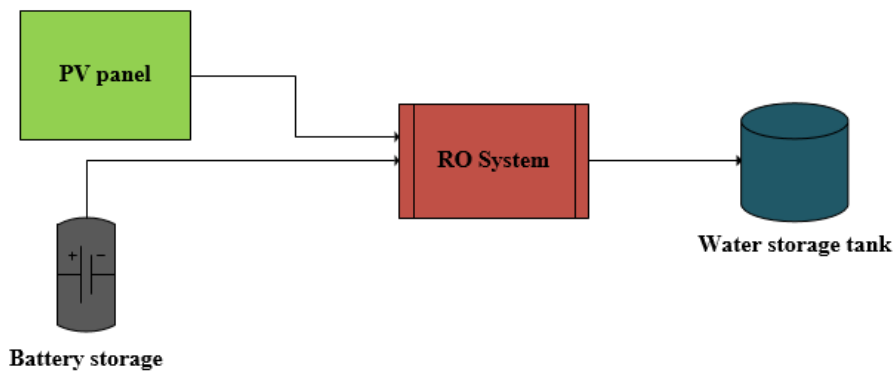
144 is designed with a larger capacity of the PV system to produce more clean water to be stored in 5 m<sup>3</sup>  
145 water tanks with an additional tank to store the excess water from the system. These two tanks are  
146 installed to back up the RO system when PV is offline. This design is the best option for RO plants  
147 driven by solar power without batteries, as proposed by Kumarasamy, Narasimhan [9]. Their  
148 experimental results showed that the optimized daily production of PV-RO without a storage tank is  
149 0.6417 m<sup>3</sup>/day, while the optimized result for PV-RO with a storage tank is 0.8682 m<sup>3</sup>/day to store  
150 two days of water production.



151  
152 **Figure 3.** Process flow of batteryless PV-RO system

### 153 2.2.2 PV-RO System with Battery Storage

154 The second scenario of the PV-RO desalination system is configured with battery installation as an  
155 energy storage system powered by solar PV. The excess energy produced from the PV plant will be  
156 stored in the battery storage system to be used later when the solar energy is unavailable to power  
157 the RO plant. The process flow of the PV-RO system with battery storage is shown in **Figure 4**.  
158 Unlike the previous configuration, this system only uses one water tank to store the water. The  
159 battery's addition means the PV-RO works longer to meet the clean water needs.

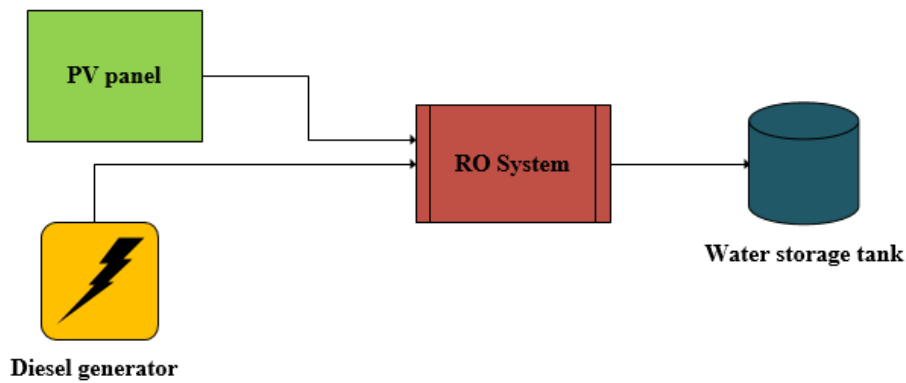


160  
161 **Figure 4.** Process flow of PV-RO system with battery storage



### 162 2.2.3 Hybrid Diesel-PV-RO System

163 In the third scenario, simulation is performed for a hybrid system of PV-diesel generation to power  
164 the RO desalination plant. This plant also does not use an additional battery storage system; only one  
165 tank is used. The energy required by the PV-RO system is supplemented with the power from the  
166 diesel generator when the PV array's electrical production is insufficient. The diesel generators also  
167 act as power backup at night time and on cloudy days to power up the RO system. **Figure 5** shows  
168 the process flow of the hybrid diesel-PV-RO system. Gökçek (2018) considered this design to  
169 integrate hybrid power involving wind, solar photovoltaic, diesel, and battery for small-scale RO  
170 desalination applications.



171  
172 **Figure 5.** Process flow of hybrid diesel/PV-RO desalination system

### 173 2.3 Energy analysis

174 The power generation capacity from PV modules to power RO system is based on the following  
175 assumptions:

- 176 • The energy requirement for the system is 3.5 kWh/m<sup>3</sup>.
- 177 • Inverter loss is 10% of the total daily energy requirement.
- 178 • Auxiliary load is 10% of the total energy and inverter loss.

#### 179 2.3.1 PV system sizing

180 The daily energy required from the PV RO system plant with system losses is given in Equation (1).

$$181 E_{load} = (E_{system} \times V) + I_{loss} + Au_{loss} \quad (1)$$

182 Where  $E_{system}$  is the energy required per cubic meter of water production (kWh/m<sup>3</sup>),  $V$  is the total  
 183 volume of daily water production from the RO system (m<sup>3</sup>),  $I_{loss}$  is inverter loss from the system  
 184 (kWh), and  $Au_{loss}$  is auxiliary loss from the system (kWh). Furthermore, the calculation of total  
 185 energy load, the electrical energy generation as an output of a photovoltaic system, can be calculated  
 186 using Equation (2).

$$187 \quad E_{tot} = E_{load} / \eta_{BOS} \quad (2)$$

188 Where  $E_{load}$  is the daily load profile calculated for the system (kWh) and  $\eta_{BOS}$  is the balance of  
 189 system efficiency (%). Thus, the energy produced by a panel is given in Equation 3 as below:

$$190 \quad E_p = A \times \eta_p \times H \quad (3)$$

191 Where  $A$  is the solar panel area (m<sup>2</sup>) and  $\eta_p$  is the panel's efficiency (%), while  $H$  is the average solar  
 192 radiation (kWh/m<sup>2</sup>/day) on tilted panels where shadings are not included. The ambient temperature  
 193 is assumed unchanged, so this study does not consider its effect on the PV. The number of required  
 194 PV panels can be calculated using Equation (4).

$$195 \quad PV_{req} = E_{tot} / E_p \quad (4)$$

196 Where  $PV_{req}$  is the number of panels required,  $E_{tot}$  is total daily energy required (kWh), and  $E_p$  is  
 197 energy produced by the panel (kWh).

### 198 **2.3.2 Diesel generator model**

199 Hybrid power systems that combine PV systems and diesel generators are essential to ensure energy  
 200 supply continuity and increase the reliability of the energy production system. Diesel generators are  
 201 used in this study to back up the power of the PV arrays due to their intermittent nature. The diesel  
 202 works when the output power from the renewable power unit does not meet the load demand. The  
 203 following Equation (5) is to define the generator capacity.

$$204 \quad E_{gen} = E_{req} \times A \quad (5)$$

205 Where  $E_{req}$  is the energy required (kWh), and  $A$  is the backup period for the generator design (%).  
 206 Moreover, Equation (6) gives the generator's fuel consumption in L/hr as a function of its electrical  
 207 output.

$$208 \quad F = F_0 \times Y_{gen} + F_1 \times P_{gen} \quad (6)$$

209 Where  $F_0$  is the intercept coefficient of the fuel curve (L/hr/kW),  $F_1$  is the fuel curve slope (L/hr/kW),  
 210  $Y_{gen}$  is the generator's rated capacity (kW) and  $P_{gen}$  is the electrical output of the generator (kW).  
 211 The values for  $F_0 = 0.246 \text{ L/kWh}$  and  $F_1 = 0.08145 \text{ L/kWh}$  [19]. The diesel fuel price is  
 212 considered flat at \$0.85/L, and there is no penalty for CO<sub>2</sub> emission.

### 213 **2.3.3 Battery sizing**

214 As the storage system of the PV-RO system due to sunshine intermittency, battery systems are  
 215 installed for energy storage and backup. The excess energy generated by PV in the peak time is used  
 216 to charge the battery until it is fully charged. However, the hybrid system uses the battery to supply  
 217 power within its allowable limit. Battery storage capacity is calculated in detail using Equation (7).

$$218 \quad E_{battery} = \frac{E_{load} \times n}{DoD \times \eta_b \times V} \quad (7)$$

219 Where  $E_{load}$  is the daily load energy profile for the system (kWh),  $\eta_b$  is the number of autonomy  
 220 days,  $DoD$  is the battery depth of discharge (%), and  $\eta$  is the battery efficiency (%). Ganora et al.  
 221 [20] found that PV-RO battery design is considered oversizing around 5-10% higher to significantly  
 222 improve the plant system, providing energy to the battery system.

### 223 **2.3.4 Inverter sizing**

224 An inverter converts the DC from PV cells to AC delivered to the RO plant. The array-to-inverter  
 225 ratio is needed to determine the sizing of the inverter, which can be measured with the DC rating of  
 226 the PV array divided by the maximum AC output of the inverter. The installation of the inverter  
 227 generally has a ratio between 1.15 to 1.25 according to the array-to-inverter ratio. The manufacturers  
 228 usually limit the ratio to 1.55 for safety and economic purposes. The more excellent output rating of

229 the inverter should be selected for safety reasons. The inverter also should be 20-30% or more  
230 significant for safety measurements. The inverter would be more efficient if running slightly higher  
231 than the overall capacity.

## 232 **2.4 Economic Analysis**

233 Economic analysis is critical in proposing an optimal renewable generation system scenario. The  
234 economic evaluation is based on the net present value (NPV) method, which uses the difference  
235 between the current value of all costs over the life of the system and the present value of all benefits  
236 over the project's useful life.

237 The value of the specific capital cost of the system in this study is assumed to be \$ 1400/(m<sup>3</sup>/d) with  
238 the costs percentage breakdown of the RO system components capital costs listed in **Table 1**, as  
239 derived from Papapetrou, Cipollina [21]. The operating costs include membrane replacement, cost  
240 of equipment maintenance, chemicals for pre-treatment and post-treatment, insurance and labor, and  
241 energy cost [22]. The system capacity influences the cost of the RO desalination system.

242 **Table 1.** Estimation of capital cost breakdown components [21]

<b>Capital cost components</b>	<b>Value (\$/(m<sup>3</sup>/d))</b>
RO modules (membrane elements and pressure vessels)	250
Other types of equipment (pumps, pre-treatment, and post-treatment include filtration and chemicals, power electronics, etc.)	450
Brackish water intake	100
Site preparation, installation, and infrastructure	400
Other costs (engineering, insurance, shipping and legal costs)	140
<b>Total</b>	<b>1,400</b>

243

244 Financial benefits are an essential aspect to be evaluated in this study whereby calculating a project's  
245 internal rate of return (IRR) and the project's return during a specific period can be determined. The

246 IRR is also used to evaluate the project's feasibility and compare scenarios. The IRR for 20 years of  
247 project lifetime can be computed through Equation (8) from [23].

$$248 \quad NPV = \sum_{n=1}^{20} CF / (1 + r)^n \quad (8)$$

249 Where  $CF$  is annual cash flow (\$),  $n$  is the number of years,  $NPV$  is the net present value (\$), and  $r$   
250 is the internal rate of return (%). NPV will be set at zero to determine the value of IRR. The  
251 discounted rate and minimum attractive rate of return (MARR) are assumed to be 10%, with no  
252 inflation and depreciation considered. The calculation of cumulative cash flow is used to understand  
253 the annual economic performance at the end of the project period.

254 Furthermore, the profit from the first year is subtracted over capital cost to calculate the cumulative  
255 cash flow, which gives the cumulative cash flow of the first year. The result is then added to the  
256 second year's cash flow gain to get the cumulative cash flow for each year and is repeated until the  
257 last year of the project. The final results show the closing cash flow after the project ends.  
258 Accordingly, the payback period and the cumulative cash flow results can be computed using  
259 Equation (9) for the discounted payback period calculation.

$$260 \quad PBP = A + B/C \quad (9)$$

261 Where  $A$  is the year with a negative discounted cumulative cash flow (year),  $B$  is the cumulative  
262 discounted cash flow in the year before recovery (\$), and  $C$  is the discounted cumulative cash flow  
263 in the year after recovery (\$).

264 Next, the Levelised Cost of Energy (LCOE) is defined as a value to assess the energy cost over the  
265 lifetime of the project. This LCOE calculates the present value of the total price per unit of electricity  
266 generated throughout the project life. Additionally, LCOE allows the comparison of different energy  
267 resources. It can be alternatively said that LCOE is the minimum price at which the electricity  
268 generated by the project is required to be sold over the total lifetime production costs. The following  
269 Equation (10) is used to calculate the LCOE.

$$270 \quad LCOE = C_{ann,tot} / E_{gen} \quad (10)$$

271 Where  $C_{ann,tot}$  is the total of the costs annualized for the power system source (\$/year) and  $E_{ser}$  is  
 272 the total electricity generated per year (kWh/year).

273 Furthermore, the Levelised Cost of Water (LCOW) needs to be considered. The LCOW defines the  
 274 cost per unit volume of water produced by a water treatment process. Lower values represent a more  
 275 efficient method as the value measures efficiency. The LCOW can be computed by using the  
 276 following Equation (11).

$$277 \quad LCOW = CAPEX + OPEX / W_{tot} \quad (11)$$

278 Where  $CAPEX$  define capital expenditure (\$),  $OPEX$  as operating and maintenance expenditure (\$)  
 279 and  $W_{tot}$  is the total water production (m<sup>3</sup>).

## 280 **2.5 Environmental Analysis**

281 Environmental analysis is vital in proposing a power generation project to monitor pollutants and  
 282 other chemicals in the atmosphere, water, and other parameters. This section will calculate and  
 283 tabulate the CO<sub>2</sub> emission for each scenario. For solar PV plant, the avoidance emission could be  
 284 computed from Equation (12).

$$285 \quad CO_2 PV = E \times e_{elec} \times t \quad (12)$$

286 Where  $E$  is the estimated annual energy generation (kWh),  $e_{elec}$  is the generic emission factor of  
 287 electricity for CO<sub>2</sub> (kg/kWh), and  $t$  is the project lifetime (years). The generic emission factor of  
 288 CO<sub>2</sub> is 0.6 kg/kWh CO<sub>2</sub>, which the Indonesian Ministry of Energy and Mineral Resources provides.  
 289 On the other hand, for hybrid diesel and PV energy generation, CO<sub>2</sub> emission reduction can be  
 290 obtained by multiplying avoidance emissions from PV and emissions produced from the diesel  
 291 generator. The formula for calculating diesel emission can be seen in Equation (13).

$$292 \quad CO_2 diesel = E \times e_{diesel} \times t \quad (13)$$

293 Where  $E$  is the estimated annual energy generation (kWh),  $e_{diesel}$  is the CO<sub>2</sub> emission factor of diesel  
 294 fuel (kg/kWh), and  $t$  is the project lifetime (years). The CO<sub>2</sub> emission factor of diesel fuel is 0.267  
 295 kg/kWh [24].

### 296 3. Results and Discussion

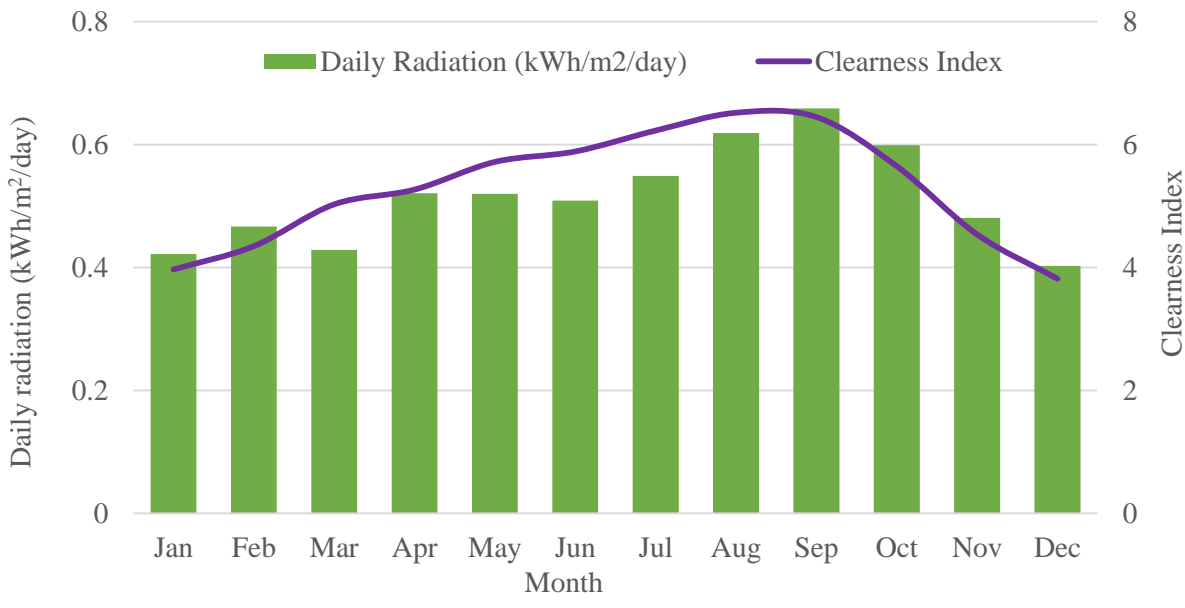
297 The basic assumption for this study is the PV-RO system has a maximum total water capacity of 5  
 298 m<sup>3</sup> per day with a daily energy requirement of 3.5 kWh/ m<sup>3</sup>. Then, the theoretical daily energy  
 299 requirement for the system is found to be 21.25 kWh/day, including inverter losses and auxiliary  
 300 loads. The total daily energy requirements for the PV-RO unit involving the auxiliaries are computed  
 301 and summarized in Table 2.

302 **Table 2.** The energy needs of the system

Type of load	Maximum power energy needs
Energy requirement	3.5 kWh/m <sup>3</sup>
Total water capacity	5 m <sup>3</sup> / day
RO daily requirement	17.5 kWh/day
RO load, including inverter losses (10%)	19.25 kWh
Auxiliary loads	2 kWh
Total energy	21.25 kWh

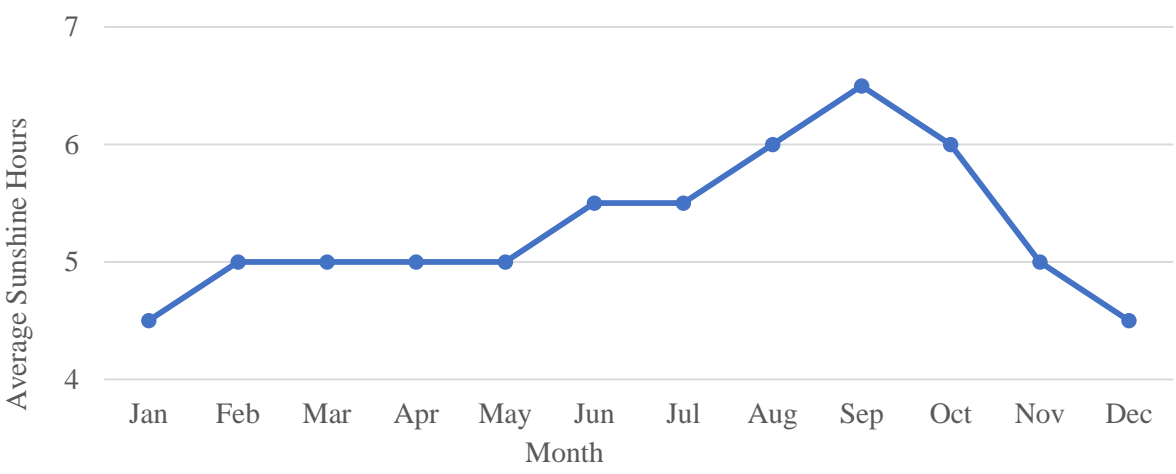
303  
 304 The PV system sizing calculation must consider the solar irradiation, sunshine hours, and site  
 305 temperature. The solar irradiation and clearness index radiation are illustrated in **Figure 6**. The  
 306 clearness index represents a measurement of the clearness of the atmosphere in which the solar  
 307 radiation factor is transmitted through the atmosphere to reach the Earth's surface. **Figure 6** shows  
 308 an increasing pattern from January to September, then decreasing in the remaining month. The  
 309 monthly radiation in the Karimunjawa islands ranges from 4.03 kWh/m<sup>2</sup> to 6.59 kWh/m<sup>2</sup>, with the  
 310 highest radiation in September and the lowest in December. The average annual radiation is 5.23  
 311 kWh/m<sup>2</sup>. Meanwhile, the clearness index shows a range between 0.382 to 0.645. The index goes the

312 highest value in September, while December is the lowest. The average peak of sunshine hours and  
 313 daily temperature are shown in **Figure 7** and **Figure 8**, respectively.



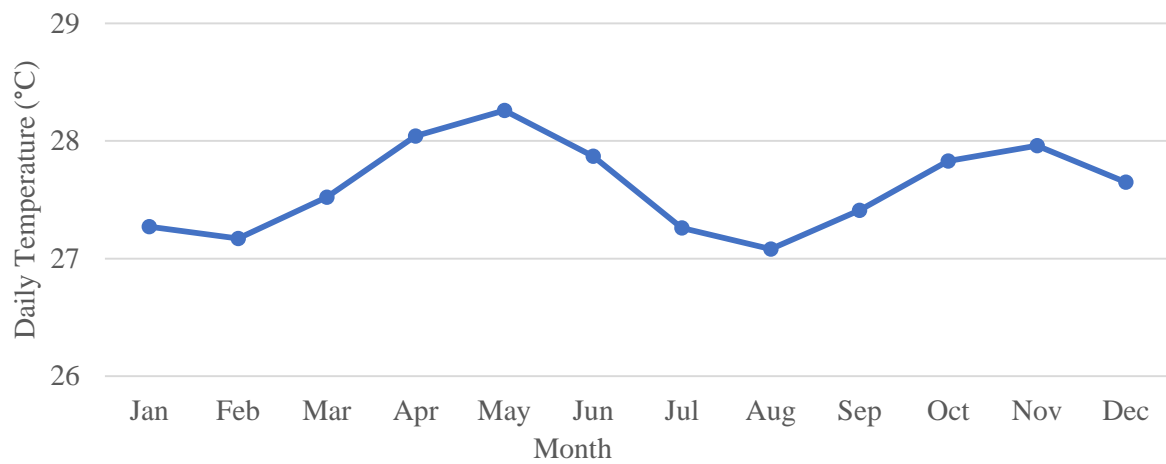
314  
 315 **Figure 6.** Monthly radiation and clearness index profile

316 Five sunshine hours are used as the optimum and annual average peak to optimize the design of the  
 317 PV-RO system. **Figure 7** depicts the average monthly sunshine hours within the range of 4.5 to 6.5  
 318 hours as the highest throughout the year. Likewise, **Figure 8** represents the average temperature for  
 319 every month, ranging from 27.08 to 28.26 °C. The highest temperature is in June, and the lowest one  
 320 is in August. The temperature is relatively stable throughout the year, with an average of 27.61 °C in  
 321 the Karimunjawa islands.



322  
 323 **Figure 7.** Monthly average sunshine hours





**Figure 8.** Monthly average daily temperature

### 3.1 Batteryless PV-RO System

In this scenario, energy generation is entirely driven by a PV system, so the energy consumption obtained from the designed RO plant is used to develop the PV requirement. The PV system is designed to have enough energy to supply the operation of the RO plant. The required PV panels are estimated based on the energy required to operate pressure pumps in the RO plant.

The capacity of the PV modules is designed so that all the water demand is produced during sunshine for about 8 hours, as this scenario did not have any backup system. Thus, the PV plant is designed to have a 20% bigger size than the typical daily energy requirement. The optimal size for the PV array is 6.3 kW, obtained from the calculation in Equation 2. Polycrystalline solar panels of LONGi LR6-72HV-350M from LONGi Solar are selected for this system, with the power rating of each module being 350 W. The power output of the PV array is a function of the average solar irradiation and the sunshine hours in Parang Island as 5 hours.

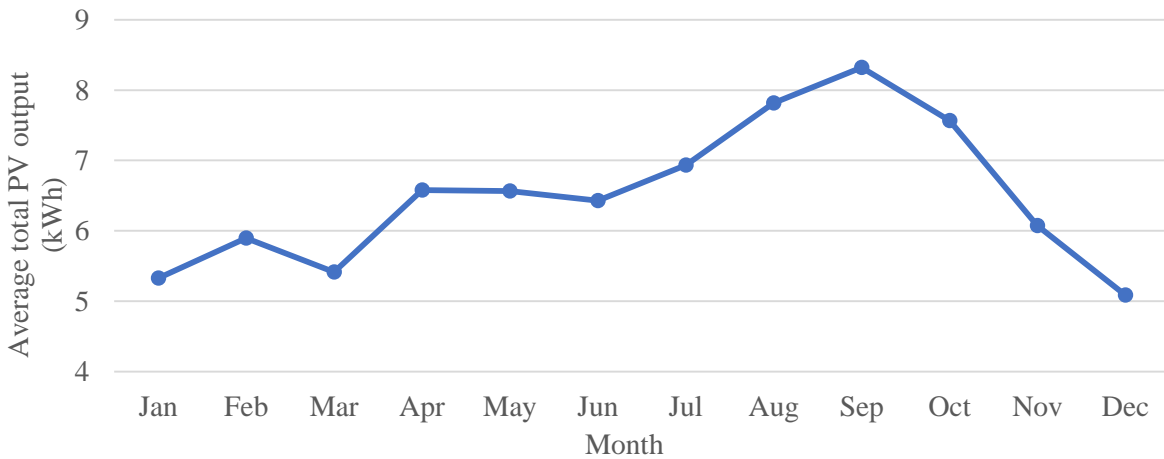
Further, a grid-tied inverter is required to connect the PV panel's DC output to the grid's AC power. Thus, a bi-directional inverter is connected between battery and load for DC/AC conversion and battery charging when there is low power from PV. Adding this inverter requires several string inverters for the PV string array. The advantages of the string inverter are reducing the combiner box and easier troubleshooting and system monitoring. In case of inverter failure, only a tiny part of the production will be lost. The inverter model of Schneider Conext XW+ 8548 E has been chosen in

344 this study with optimal efficiency of 96%. The technical parameters for PV, converter, and battery  
 345 considered in this RO design are shown in **Table 3**.

346 **Table 3.** Technical parameters for Scenario 1

PV		Converter	
Factors	Value	Factors	Value
Model	LONGi LR6-72HV-350M	Model	Schneider Conext XW+ 8548 E
Maximum power	350 W	Lifetime	15 years
Dimensions (L*W*H)	1956×991×45 mm	Efficiency	96%
Module efficiency	18.1%	Output power	7000 W
Derating factor	90%	Input DC voltage range	40 to 64 V (43 V nominal)
Lifetime	25 years	Maximum input DC current	180 A

347  
 348 The calculated energy generation from the PV system can be seen in **Figure 9**. The designed PV  
 349 system has a 20% bigger size than the daily energy load to ensure enough electricity to power the  
 350 RO system. **Figure 9** shows that the PV output ranges between 5.09 kW to 8.32 kW, with the lowest  
 351 month in December and the highest in September. This scenario does not install a battery or diesel  
 352 system. The additional tank is installed to store the overproduction of water and used during uncertain  
 353 weather later.



354  
 355 **Figure 9.** Energy generation from PV system for Scenario 1

356 This study presents the economic analysis for three different scenarios compared to the standalone  
 357 diesel-powered RO system. From an economic point of view, using an RO plant and PV system  
 358 together could reduce desalinated water costs. **Table 4** represents the financial data for the power  
 359 system considered.

360 **Table 4.** Economic parameters for Scenario 1

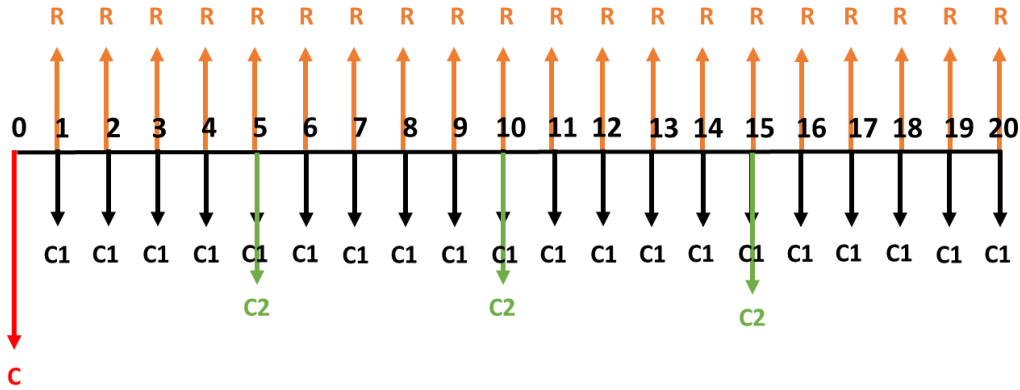
No	System component	Unit	Price
<b>1.</b>	<b>RO plant</b>		
	Capital cost	\$	7,500.00
	Operation and maintenance	\$/year	350
	Projected lifetime	year	20
<b>2.</b>	<b>PV unit</b>		
	Capital cost	\$/unit	350.00
	Operation and maintenance	\$/year	10.00
<b>3.</b>	<b>Converter</b>		
	Capital cost	\$/unit	1,500.00
	Replacement cost	\$/unit	1,300.00
	Operation and maintenance	\$/year	10

361

362 A cash flow diagram visually represents income and expenses over some project lifetimes is required  
 363 to analyze the economic impact further. The details of the cash flow diagram of Scenario 1 are given  
 364 as detailed in **Figure 10**, where the downwards arrow defines the cost associated with the project or  
 365 negative cash flow and upwards arrow C for the positive cash flow. In **Figure 10**, the capital cost is  
 366 symbolized by C, while C1 is the O&M cost during the project lifetime, which shows the same value,  
 367 and C2 is the replacement of equipment costs. The first and second replacements will be in the years  
 368 5 and 10 for auxiliaries, where replacement in year 15 is for auxiliaries and converter. There is R for  
 369 revenue or profit the project will obtain annually on the positive cash flow side. Thus, under Scenario  
 370 1, using the discounted rate of 10%, each component cost is broken down in Table 5 shows three

371 cost components: the RO system, the PV panel, and the converter. More than 80% of the total costs  
 372 associated with the RO system include auxiliaries, while the other 20% are from PV panel and  
 373 converter costs. Scenario 1 resulted in a total NPV of \$ 21,143.1.

374 **Table 5.**



375

376 **Figure 10.** Cash flow diagram of Scenario 1

377 Table 5 shows three cost components: the RO system, the PV panel, and the converter. More than  
 378 80% of the total costs associated with the RO system include auxiliaries, while the other 20% are  
 379 from PV panel and converter costs. Scenario 1 resulted in a total NPV of \$ 21,143.1.

380 **Table 5.** Net present value of each component for Scenario 1

Component	Capital	Replacement	O&M	Total
RO system	\$ 7,500.00	934.35	2,979.90	11,414.25
PV panel	\$ 6,300.00		1,532.52	7,832.52
Converter	\$ 1,500.00	311.22	85.14	1,896.36
<b>Total NPV</b>				<b>21,143.1</b>

381

382 Further, the details of economic performance for Scenario 1 are given in **Table 6** to depicts the annual  
 383 cash flow of the project involving capital cost, operation and maintenance (O&M) cost, replacement  
 384 cost, annual savings, and annual profit. The capital cost is \$ 24,900.00, with a yearly O&M cost of  
 385 \$ 690.00. There are two replacement costs: auxiliary replacement accounted for every five years and

386 converter replacement in year 15. With the amount of energy generation from PV, the annual saving  
 387 was \$ 2326.88 per year from diesel savings. Meanwhile, yearly profit was taken from drinking water  
 388 sold to the inhabitants.

389 **Table 6.** Annual economic performance of Scenario 1 in USD (\$)

Year	Capital cost	O&M	Replacement cost	Annual saving	Annual profit	Cash flow	Cumulative cash flow
0	15,300.00					15,300.00	-15,300.00
1		540.00		2,326.88	1,775.65	3,562.53	-11,737.48
2		540.00		2,326.88	1,775.65	3,562.53	-8,174.95
3		540.00		2,326.88	1,775.65	3,562.53	-4,612.43
4		540.00		2,326.88	1,775.65	3,562.53	-1,049.90
<b>5</b>		<b>540.00</b>	<b>750.00</b>	<b>2,326.88</b>	<b>1,775.65</b>	<b>2,812.53</b>	<b>1,762.63</b>
6		540.00		2,326.88	1,775.65	3,562.53	5,325.15
7		540.00		2,326.88	1,775.65	3,562.53	8,887.68
8		540.00		2,326.88	1,775.65	3,562.53	12,450.20
9		540.00		2,326.88	1,775.65	3,562.53	16,012.73
10		540.00	750.00	2,326.88	1,775.65	2,812.53	18,825.25
11		540.00		2,326.88	1,775.65	3,562.53	22,387.78
12		540.00		2,326.88	1,775.65	3,562.53	25,950.30
13		540.00		2,326.88	1,775.65	3,562.53	29,512.83
14		540.00		2,326.88	1,775.65	3,562.53	33,075.35
15		540.00	2,050.00	2,326.88	1,775.65	1,512.53	34,587.88
16		540.00		2,326.88	1,775.65	3,562.53	38,150.40
17		540.00		2,326.88	1,775.65	3,562.53	41,712.93
18		540.00		2,326.88	1,775.65	3,562.53	45,275.45
19		540.00		2,326.88	1,775.65	3,562.53	48,837.98
20		540.00		2,326.88	1,775.65	3,562.53	52,400.50

390  
 391 After calculating cumulative cash flow, the simple payback period and discounted payback period  
 392 are given in year 6 of the project lifetime. Hence, to determine the system's energy and water cost,  
 393 LCOE for Scenario 1 is \$ 0.154/kWh, with the LCOW of \$ 0.627/m<sup>3</sup>. This result is slightly lower

394 than the study by Subedi [25] for the solar-powered RO desalination system analysis. He presented  
395 a design to produce 12 m<sup>3</sup> of water per day, and the water desalination cost from the PV-RO plant  
396 was estimated to be around \$0.67/m<sup>3</sup>.

397 Furthermore, for the environmental aspect, it is essential to switch fossil fuels with renewable energy  
398 resources to decrease the carbon footprint and greenhouse gas emissions. The use of solar energy as  
399 a source of electricity in an RO plant consequently saves fossil fuel. This study examined the  
400 operational emissions of the hybrid power system and did not compute associated emissions with the  
401 production of the equipment used. Since the study only measures emissions generated by diesel  
402 generators in the hybrid power generation, Scenario 1 considered not emitting any pollutants because  
403 renewable sources power 100% of the operation.

404 However, this scenario's annual CO<sub>2</sub> emission reduction can be computed with the 111,690 kg CO<sub>2</sub>  
405 equivalent and 20 years project lifetime based on the Indonesian electricity emission factor or about  
406 six metric tons per annum. This figure is lower than the finding by Subedi [25], which estimated to  
407 save approximately ten metric tons of CO<sub>2</sub> per annum. This difference in results is mainly due to the  
408 different sizing systems. Subedi [25] analyzed a PV-RO system with a capacity of 12 m<sup>3</sup>, while the  
409 present study calculated it for a capacity of 5 m<sup>3</sup>. In contrast, this result is consistent with the previous  
410 statement that the sizing system will affect the overall analysis, resulting in economic and  
411 environmental benefits.

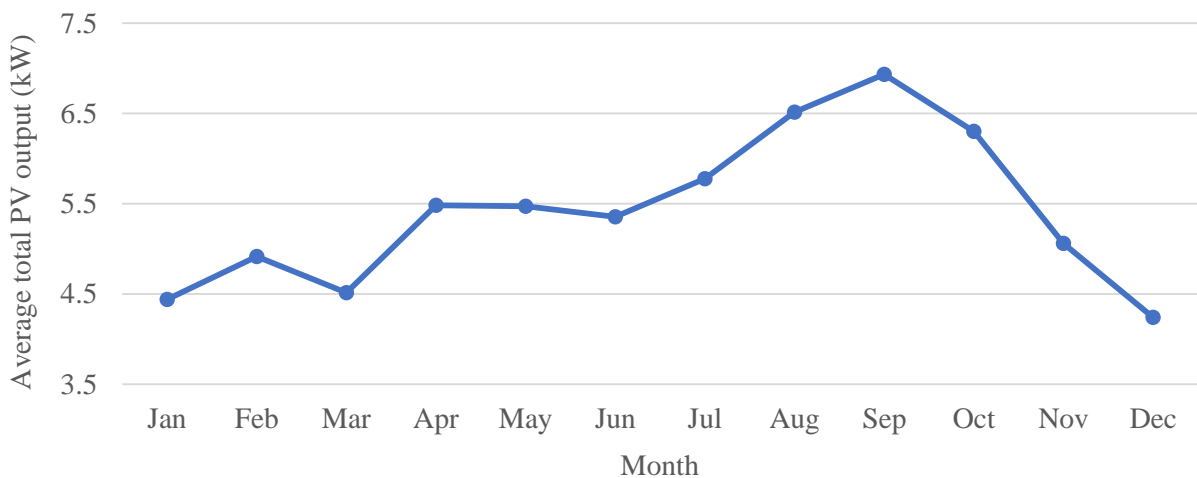
### 412 **3.2 PV-RO System with Battery Storage**

413 This second scenario has an energy configuration of a PV system as the primary energy generation  
414 source and battery storage as a backup system when sunshine is unavailable during certain times.  
415 The total energy required for Scenario 2 was found to be 5.25 kW on the PV array. This project  
416 selects Polycrystalline solar panels of LONGi LR6-72HV-350M from LONGi Solar with an  
417 efficiency of up to 18.1%. As the storage system, battery type selection will affect the designed  
418 system lifetime depending on the number of operation cycles. The battery type considered is a 12 V  
419 lead-acid battery of Discover 12VRE-3000TF for this PV-RO system design because of its

420 reasonable cost. To convert DC to AC load, the inverter model of Schneider Conext XW+ 7048 E  
 421 has been chosen in this study with output rated AC power 6000 W with optimal efficiency of 96%.  
 422 To sum up, the technical parameters for PV, converter, and battery considered in this RO design are  
 423 shown in **Table 7**, while the renewable generation can be seen in **Figure 11**.

424 **Table 7.** Technical parameters for Scenario 2

PV		Battery	
Factors	Value	Factors	Value
Model	LONGi LR6-72HV-350M	Model	Discover 12VRE-3000TF
Maximum power	350 W	Nominal voltage	12 V
Dimensions (L*W*H)	1956×991×45 mm	Nominal capacity	3.11 kWh
Module efficiency	18.1%	Maximum capacity	220 Ah
Derating factor	90%	Capacity ratio	0.563
Lifetime	25 years	Maximum charge current	43 A
Converter			
Factors		Value	
Model		Schneider Conext XW+ 7048 E	
Lifetime		15 years	
Efficiency		96%	



425 **Figure 11.** Energy generation from PV system for Scenario 2  
 426

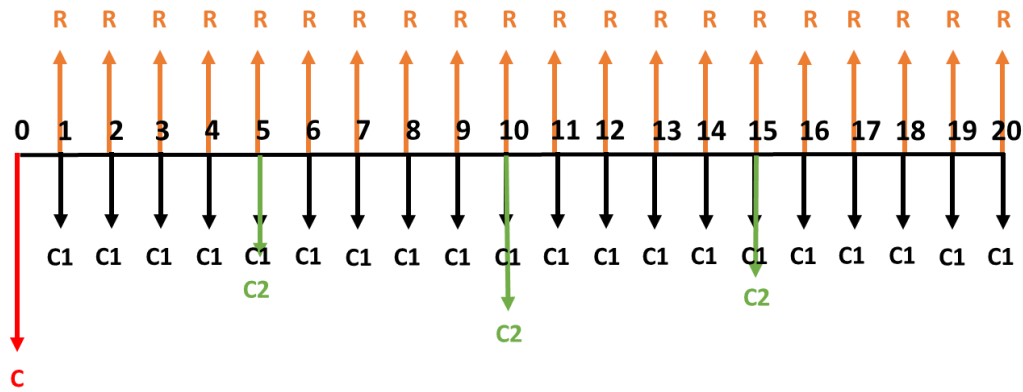
427 As shown in **Figure 11**, the energy output from the PV system started from 4.24 kWh in December  
 428 and increased slightly until September, delivering the highest energy generation of 6.93 kWh. The  
 429 remaining month shows a decreasing pattern up to the lowest energy produced in December of 4.24  
 430 kWh due to the daily solar radiation throughout the year. Ganora, Hospido [20] stated that this energy  
 431 created is enough for energy storage options for PV-RO desalination. They found that the average  
 432 energy requirement for PV-RO with batteries is approximately 3.3 kWh/m<sup>3</sup>. This comparison shows  
 433 that the proposed system required reasonably higher energy. However, a similar finding is reported  
 434 by Karimanzira [26] in the research of wind-powered RO desalination plants that a system that uses  
 435 energy storage and optimization requires at least a specific Energy of 6.34 KWh/m<sup>3</sup>. In addition,  
 436 using an RO plant and PV system together reduces desalinated water costs. This study presents the  
 437 economic analysis for three different scenarios compared to RO powered by a diesel generator. **Table**  
 438 **8** represents the financial data for the power system considered, while the system cash flow diagram  
 439 is detailed in **Figure 12** to provide more detail on the annual cost.

440 **Table 8.** Economic performance of Scenario 2

No	System component	Unit	Price
<b>1.</b>	<b>RO plant</b>		
	Capital cost	\$	7,000.00
	Operation and maintenance	\$/year	350
	Projected lifetime	year	20
<b>2.</b>	<b>PV unit</b>		
	Capital cost	\$/unit	350.00
	Operation and maintenance	\$/year	10.00
<b>3.</b>	<b>Batteries</b>		
	Capital cost	\$/unit	300.00
	Operation and maintenance cost	\$/unit/year	5.00
	Replacement cost	\$/unit	300.00
<b>4.</b>	<b>Converter</b>		
	Capital cost	\$/unit	1400.00



No	System component	Unit	Price
	Replacement cost	\$/kW	1300.00
	Operation and maintenance	\$/year	10



**Figure 12.** Cash flow diagram of Scenario 2.

The diagram presents opposite arrows that define a negative value or cost for the downside arrow and a positive value or revenue for the upside arrow. A negative value represents all costs during useful project life, including capital cost (C) at the beginning year, annual O&M costs (C1), and replacement which takes place in the years 5, 10, and 15 (C2). This project has the same revenue or profit (R), shown by an upwards arrow. Hence, each component cost can be breakdown using a discounted rate of 10% in **Table 9**.

**Table 9.** Net present value of each component for Scenario 2.

Component	Capital	Replacement	O&M	Total
<b>RO system</b>	7,000.00	872.06	2,979.90	10,851.96
<b>PV panel</b>	5,250.00		1,277.10	6,527.10
<b>Battery</b>	3,720.00	2,309.75	510.84	6,346.08
<b>Converter</b>	1,400.00	1,300.00	85.14	2,785.14
<b>Total NPV</b>				<b>26,510.28</b>

As shown in **Table 9**, there are four components: costs of RO system, PV panel, battery, and converter. Each part consists of capital, replacement, and operation and maintenance costs, and all expenses are considered to net present value. The highest cost was found for the RO system at \$

454 10,851.96, while the PV panel and battery costs slightly differ between \$ 6,527.10 and \$ 6,346.08,  
455 respectively. The converter was the least cost that was accounted for \$ 2,785.14. In total, the net  
456 present value for Scenario 2 was \$ 26,510.28. This cost agrees with the study by Ganora, Hospido  
457 [20] that a PV-RO desalination plant equipped with batteries and reservoir storage has about 1.2  
458 times higher investment costs. Accordingly, the details of economic performance for Scenario 2 are  
459 given in **Table 10**. It can be seen that the payback period for Scenario 2 will be around six years.  
460 However, the IRR shall also be computed as a guideline for proceeding with a project or investment.  
461 IRR for this scenario is 15.92%, LCOE is \$ 0.174/kWh, and LCOW of \$ 0.686/m<sup>3</sup>.

462 **Table 10.** Annual economic performance for Scenario 2 in USD (\$).

Year	Cost	O&M	Replacement cost	Annual saving	Annual profit	Cash flow	Cumulative cash flow
0	17,250.00					17,250.00	17,250.00
1		570.00		2,326.88	1,668.63	3,425.50	13,824.50
2		570.00		2,326.88	1,668.63	3,425.50	10,399.00
3		570.00		2,326.88	1,668.63	3,425.50	-6,973.50
4		570.00		2,326.88	1,668.63	3,425.50	-3,548.00
5		570.00	700.00	2,326.88	1,668.63	2,725.50	-822.50
<b>6</b>		<b>570.00</b>		<b>2,326.88</b>	<b>1,668.63</b>	<b>3,425.50</b>	<b>2,603.00</b>
7		570.00		2,326.88	1,668.63	3,425.50	6,028.50
8		570.00		2,326.88	1,668.63	3,425.50	9,454.00
9		570.00		2,326.88	1,668.63	3,425.50	12,879.50
10		570.00	4,300.00	2,326.88	1,668.63	-874.50	12,005.00
11		570.00		2,326.88	1,668.63	3,425.50	15,430.50
12		570.00		2,326.88	1,668.63	3,425.50	18,856.00
13		570.00		2,326.88	1,668.63	3,425.50	22,281.50
14		570.00		2,326.88	1,668.63	3,425.50	25,707.00
15		570.00	2,000.00	2,326.88	1,668.63	1,425.50	27,132.50
16		570.00		2,326.88	1,668.63	3,425.50	30,558.00
17		570.00		2,326.88	1,668.63	3,425.50	33,983.50

Year	Cost	O&M	Replacement cost	Annual saving	Annual profit	Cash flow	Cumulative cash flow
18		570.00		2,326.88	1,668.63	3,425.50	37,409.00
19		570.00		2,326.88	1,668.63	3,425.50	40,834.50
20		570.00		2,326.88	1,668.63	3,425.50	44,260.00

463

464 From the environmental view, this scenario does not produce any emissions during operation time  
465 because it has fully solar-driven energy generation. However, CO<sub>2</sub> emission reduction can be  
466 computed from the electricity emission factor of using fossil fuels. This PV-RO configuration  
467 avoided 93,075 kg CO<sub>2</sub> equivalent emission to the atmosphere.

### 468 3.3 Hybrid Diesel-PV-RO System

469 The last scenario is the hybrid diesel-PV-RO plant with a daily capacity of 5 m<sup>3</sup>/day. The PV model  
470 is LONGi LR6-72HV-350M, with 12 panels with a total capacity of 4.2 kW, while the diesel  
471 generator power output is 5 kW with total fuel consumption of 963.6 L/year. The diesel generator of  
472 Generac GP5000 is used to back up the PV array system. The Schneider Conext SW4048 is also  
473 used in this configuration with a capacity of 4000 W and an efficiency of 94%. The technical  
474 parameters for PV, converter, and battery considered in this RO design are shown in **Table 11**, while  
475 the annual energy generation is estimated in **Figure 13**.

476

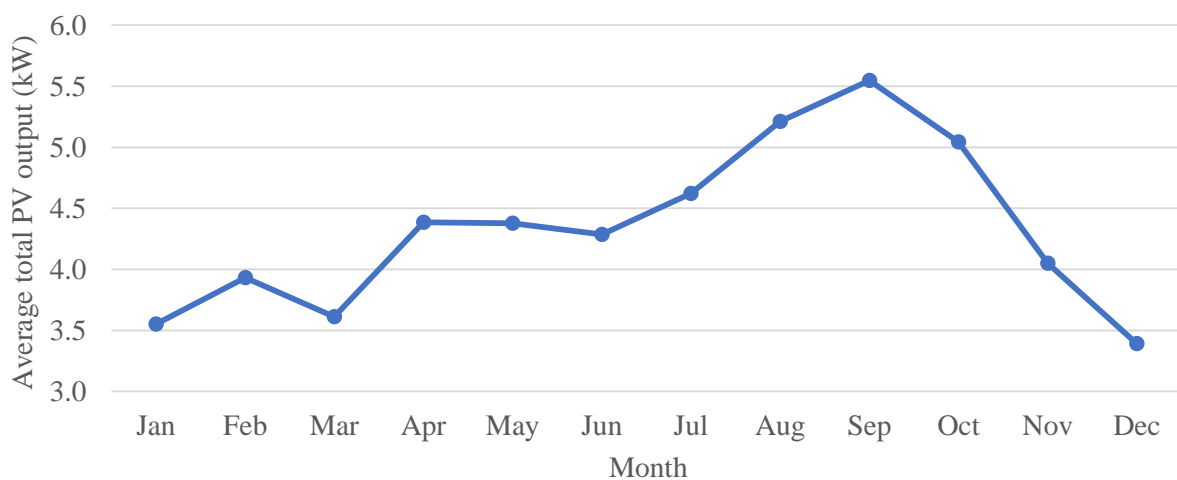
**Table 11.** Technical parameters for Scenario 3.

<b>PV</b>		<b>Diesel Generator</b>	
Factors	Value	Factors	Value
Model	LONGi LR6-72HV-350M	Model	Generac GP5000
Maximum power	350 W	Lifetime	10 years
Open circuit voltage (Voc/V)	46.9	AC rated output	5000 W
Short circuit current (Isc/A)	9.68	<b>Converter</b>	
Dimensions (L*W*H)	1956×991×45 mm	Factors	Value

PV		Diesel Generator	
Factors	Value	Factors	Value
Module efficiency	18.1%	Model	Schneider Conext SW4048
Derating factor	90%	Lifetime	15 years
Lifetime	25 years	Efficiency	95%

477

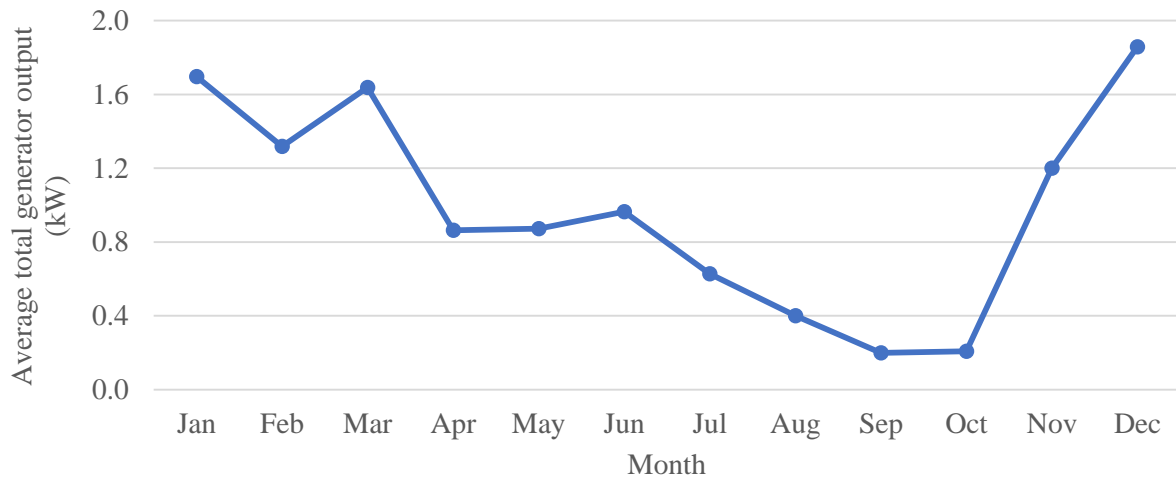
478 Less solar irradiance in September and October results in high consumption from the diesel  
479 generator. **Figure 13** illustrates the energy output of the PV system by monthly average data. The  
480 total energy lies within the range of 3.39 to 5.54 kW. However, the average total generator output  
481 shown in **Figure 14** is between 0.20 kW to 1.86 kW. The highest production lies in December while  
482 the lowest is in September, opposite the solar PV output. This result agrees with the study by Gökçek  
483 [27] for RO powered by hybrid wind, solar photovoltaic, diesel, and battery. In this study, water  
484 production capacity was 24 m<sup>3</sup>/day with an energy requirement of 4.38 kWh/m<sup>3</sup>. This energy  
485 consumption is still relatively high even with the advantages of reliable operation. This system can  
486 be optimized further by changing the design and setting the maintenance and production schedule  
487 proposed by Al-Obaidi, Rasn [17], which achieves a low energy consumption of as low as 3,755  
488 kWh/m<sup>3</sup>.



489

490 **Figure 13.** Energy generation from PV system for Scenario 3

491



492

493

**Figure 14.** Energy generation from diesel generator for Scenario 3

494

The details of each cost associated are needed to analyze the economic impact of Scenario 3. **Table**

495

**12** gives details of financial data for the power system considered, while the cash flow diagram of

496

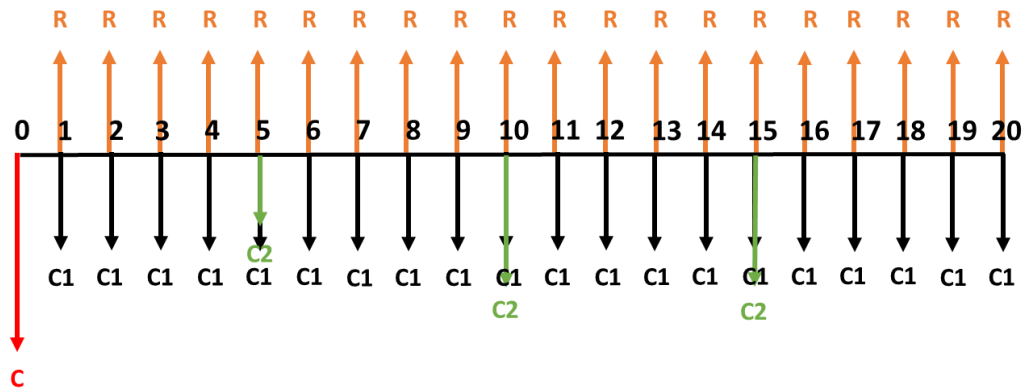
Scenario 3 is detailed in **Figure 15**.

497

**Table 12.** Economic parameters for Scenario 3.

No	System component	Unit	Price
<b>1.</b>	<b>RO plant</b>		
	Capital cost	\$	7,000.00
	Operation and maintenance	\$/year	350
	Projected lifetime	year	20
<b>2.</b>	<b>PV unit</b>		
	Capital cost	\$/unit	350.00
	Operation and maintenance	\$/year	10.00
<b>3.</b>	<b>Diesel generator</b>		
	Capital cost	\$/unit	1,200.00
	Replacement cost	\$/unit	1,200.00
	Operation and maintenance	\$/hour	0.030
	Diesel fuel price	\$/L	0.85
<b>4.</b>	<b>Converter</b>		
	Capital cost	\$/unit	1,200.00

No	System component	Unit	Price
	Replacement cost	\$/unit	1,200.00
	Operation and maintenance	\$/year	10



498

499

**Figure 15.** Cash flow diagram of Scenario 3.

500 As shown in **Figure 15**, cash out consists of capital, annual operating, and replacement costs for  
501 auxiliaries every five years, and converter and generator replacement. Cash in is expected to be a  
502 constant revenue throughout the project lifetime. Correspondingly, using a discounted rate of 10%,  
503 each component cost is broken down in **Table 13**. PV panel and converter costs accounted for 15%  
504 of the total NPV for Scenario 3 of \$ 26,377.99. It can be seen in **Table 13** that the highest cost is  
505 contributed by the RO system of \$ 10,851.96, followed by a generator.

506

**Table 13.** Net present value of each component for Scenario 3

Component	Capital	Replacement	O&M	Total
RO system	7,000.00	872.06	2,979.90	<b>10,851.96</b>
PV panel	4,200.00	-	1,021.68	<b>5,221.68</b>
Generator	1,200.00	-	6,619.21	<b>7,819.21</b>
Converter	1,200.00	1,200.00	85.14	<b>2,485.14</b>
<b>Total NPV</b>				<b>26,377.99</b>

507

508 The diesel generator has a low capital cost, but a significant fuel cost increases the total generator  
509 cost by up to \$ 7,819.21. Further, the details of economic performance for Scenario 3 are given in

510 **Table 14.** The discounted payback period was found in year 7 of the project, while IRR for this  
 511 scenario was found to be 13.42%. Therefore, Scenario 3 generates a value of \$ 0.165/kWh for LCOE  
 512 and \$ 1.036/m<sup>3</sup> for LCOW. This result is way lower than the previous study by Gökçek [27] that the  
 513 PV-wind-diesel hybrid system had a reasonable electricity cost with a value of \$0.308/kWh.

514 **Table 14.** Annual economic performance of Scenario 3

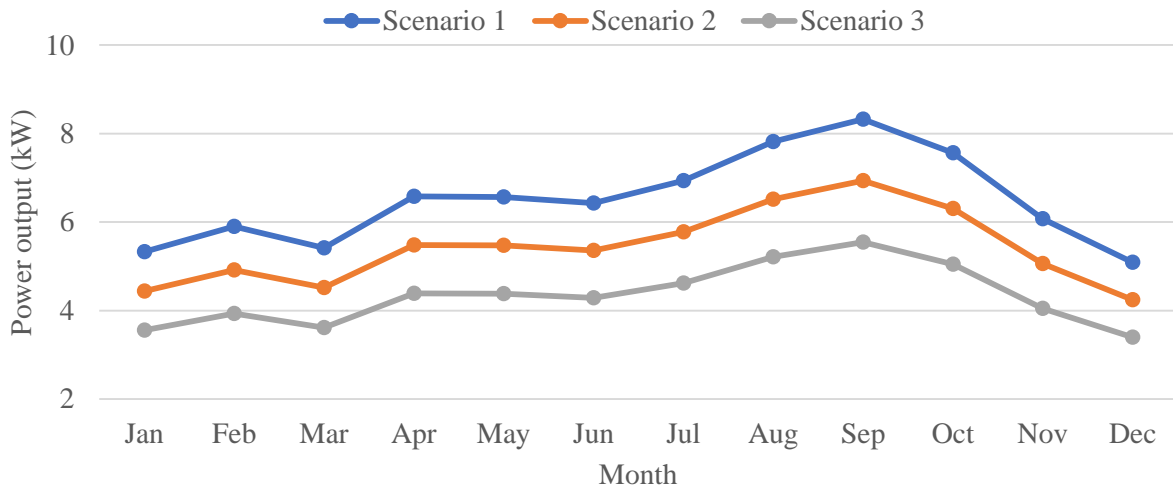
Year	Cost	O&M	Replacement cost	Annual saving	Annual profit	Cash flow	Cumulative cash flow
0	13,600.00					13,600.00	-13,600.00
1		-1,353.81		2,326.88	1,028.99	2,002.06	-11,597.95
2		-1,353.81		2,326.88	1,028.99	2,002.06	-9,595.89
3		-1,353.81		2,326.88	1,028.99	2,002.06	-7,593.84
4		-1,353.81		2,326.88	1,028.99	2,002.06	-5,591.78
5		-1,353.81	700.00	2,326.88	1,028.99	1,302.06	-4,289.73
6		-1,353.81		2,326.88	1,028.99	2,002.06	-2,287.67
7		-1,353.81		2,326.88	1,028.99	2,002.06	-285.61
<b>8</b>		<b>-1,353.81</b>		<b>2,326.88</b>	<b>1,028.99</b>	<b>2,002.06</b>	<b>1,716.44</b>
9		-1,353.81		2,326.88	1,028.99	2,002.06	3,718.50
10		-1,353.81	1,900.00	2,326.88	1,028.99	102.06	3,820.55
11		-1,353.81		2,326.88	1,028.99	2,002.06	5,822.61
12		-1,353.81		2,326.88	1,028.99	2,002.06	7,824.66
13		-1,353.81		2,326.88	1,028.99	2,002.06	9,826.72
14		-1,353.81		2,326.88	1,028.99	2,002.06	11,828.77
15		-1,353.81	1,900.00	2,326.88	1,028.99	102.06	11,930.83
16		-1,353.81		2,326.88	1,028.99	2,002.06	13,932.88
17		-1,353.81		2,326.88	1,028.99	2,002.06	15,934.94
18		-1,353.81		2,326.88	1,028.99	2,002.06	17,936.99
19		-1,353.81		2,326.88	1,028.99	2,002.06	19,939.05
20		-1,353.81		2,326.88	1,028.99	2,002.06	21,941.10

515

516 The diesel generator is a hybrid power system to power the RO plant if solar sources are unavailable  
 517 in this scenario. However, the diesel generator operation will emit CO<sub>2</sub>, CO, SO<sub>2</sub>, NO<sub>x</sub>, unburned  
 518 hydrocarbons, and particulate matter. This study has examined the CO<sub>2</sub> emission produced by the  
 519 generator as the operational emissions of the hybrid power system but did not compute associated  
 520 emissions with the production of the equipment used. With the assistance of PV generation, this  
 521 system can save 65,152 kg.CO<sub>2</sub>eq of carbon dioxide emission to the atmosphere. Nevertheless,  
 522 power generation usage also emits such amount of carbon dioxide. With a diesel emission factor of  
 523 0.267 kg/kWh, the average total energy requirement of 6.375 kWh/day may produce 12,425  
 524 kg.CO<sub>2</sub>eq. Total emission reduction is the subtraction number of avoidance electricity and diesel  
 525 emission. Thus, carbon dioxide emission of 52,727 kg.CO<sub>2</sub>eq can be avoided using this configuration  
 526 system.

527 **3.4 Comparison Between Scenarios**

528 The primary energy generation for three different scenarios comes from the PV system. The average  
 529 monthly output is compared in **Figure 16**. As illustrated in **Figure 16**, three scenarios have a similar  
 530 pattern. Each configuration system requires the same amount of energy to run the desalination system  
 531 in the condition of having the same solar exposure.

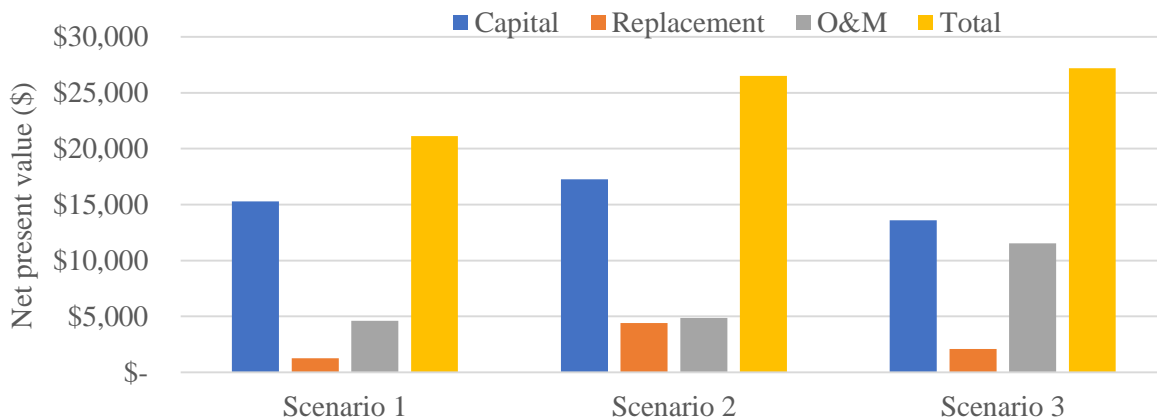


532  
 533 **Figure 16.** Comparative energy performance among scenarios



534 However, the first two scenarios have 100% renewable penetration, while Scenario 3 has a hybrid  
 535 system with a diesel generator. Scenario 1 has a 6.3 kW PV array, the highest among the three. As a  
 536 result, it produces substantial power throughout the year. Following Scenario 2, which has a 5.25  
 537 kW PV array and energy ranges from 4.24 to 6.93 kW. The least amount of energy produced from  
 538 PV is from Scenario 3 in a 3.5 kW PV configuration, in which a diesel generator assists in creating  
 539 enough power.

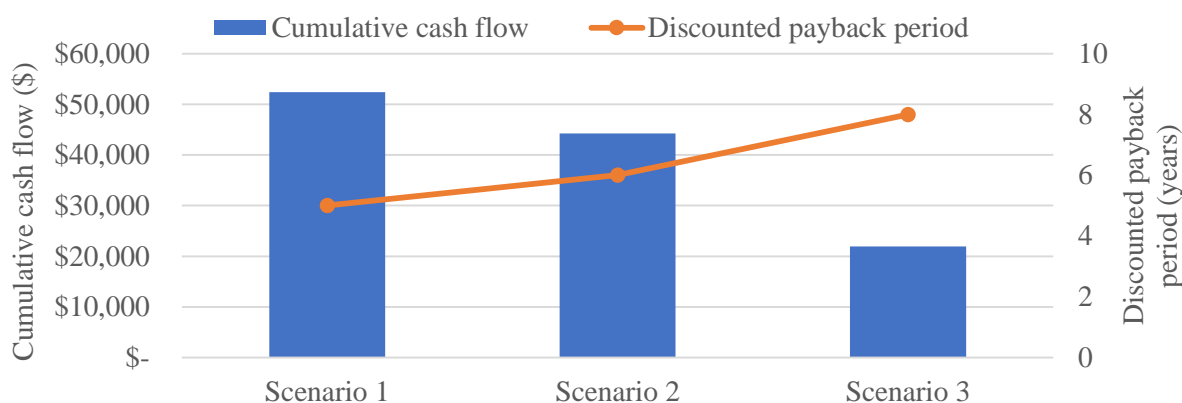
540 After determining the economic performance for each scenario, an NPV comparison is presented in  
 541 **Figure 17** to analyze the economic impact of each project. According to the results, Scenario 3 has  
 542 the lowest capital cost at \$ 13,600.00. However, in the case of diesel generator assisted, the fuel price  
 543 significantly affects the economy, which generates the highest O&M costs among scenarios of up to  
 544 \$ 11,526.34. In Scenario 2, the PV coupled with the battery storage system has the most increased  
 545 capital cost of \$ 17,250.00 due to battery installation. Likewise, the replacement cost was also highest  
 546 at \$ 4,407.30 as the batteries that contribute considerable cost need to be replaced in the middle of  
 547 the project lifetime.



548 **Figure 17.** Comparative net present value among scenarios

549  
 550 On the other hand, the batteryless configuration PV-RO system in Scenario 1 yields the lowest  
 551 replacement cost and O&M of \$ 1,245.57 and \$ 4,597.56, respectively. Therefore, from all the  
 552 different costs associated with each scenario, Scenario 3 has the highest total NPV of \$ 27,198.40,  
 553 followed by Scenario 2, which generated \$ 26,510.28, and Scenario 1 became the least at only \$

554 21,143.13. Concurrently, the economic performance of each design can be compared in which the  
 555 comparison of results are shown in **Table 15** and **Figure 18**.



556

557 **Figure 18.** Comparison of cumulative cash flow and payback period among scenarios

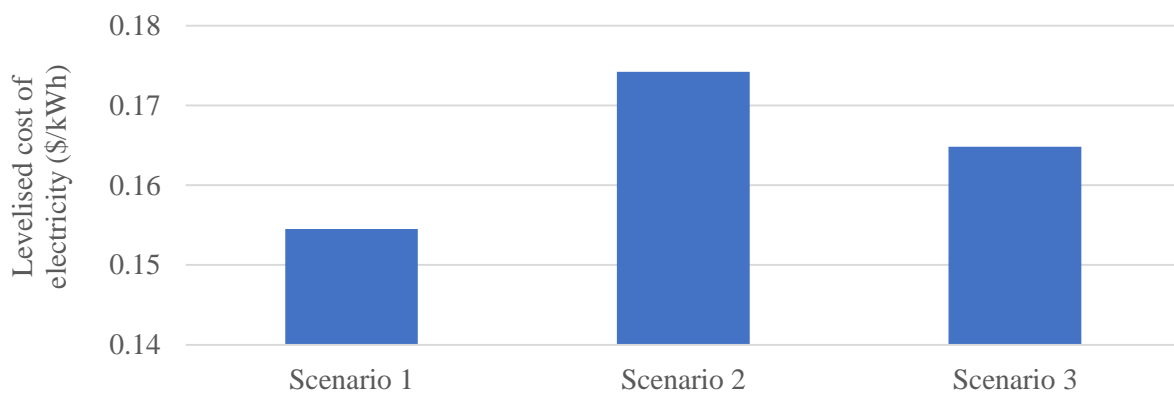
558 From **Figure 18**, the cumulative cash flow is a reverse function of discounted payback period. The  
 559 Batteryless PV-RO system scenario has the highest cumulative cash flow of \$ 52,400.50 and yields  
 560 the least payback period in five years. On the other side, the diesel-assisted PV-RO plant produced  
 561 only \$ 21,941.10 and had a longer discounted payback period of up to 8 years. This calculation shows  
 562 that installing a storage system is beneficial for the PV-RO plant.

563 Apart from cumulative cash flow and discounted payback period, the IRR of various configuration  
 564 system scenarios also needs to be examined to evaluate investment feasibility. The higher IRR  
 565 computed in a project indicates more significant net cash flows can be generated, making the project  
 566 more profitable and feasible to proceed with. As shown in **Table 15**, it can be interpreted that lower  
 567 IRR yielded as a result of either high capital or operating expenditure. The scenario when the PV-  
 568 RO system did not install with the battery system gave the highest IRR.

569 **Table 15.** Comparison of internal rate of return value among scenarios

Project Scenario	IRR
Scenario 1	21.83%
Scenario 2	15.92%
Scenario 3	12.00%

570 **Figure 19** is used to compare the Levelized cost of electricity and water. Those values range from  
 571 the scenario projection of the cost of solar electricity generation tariffs by 2030 of \$ 0.06 to \$  
 572 0.22/kWh [28]. **Figure 19** shows the LCOE values for all scenarios considered. As seen in **Figure**  
 573 **19**, each scenario slightly differs from the others. The lowest LCOE of \$ 0.154/kWh is as Scenario  
 574 1 value, while the highest LCOE value of \$ 0.174/kWh from Scenario 2 is due to the high cost of  
 575 batteries. This comparison is a 2% increment compared to a batteryless PV-RO plant.

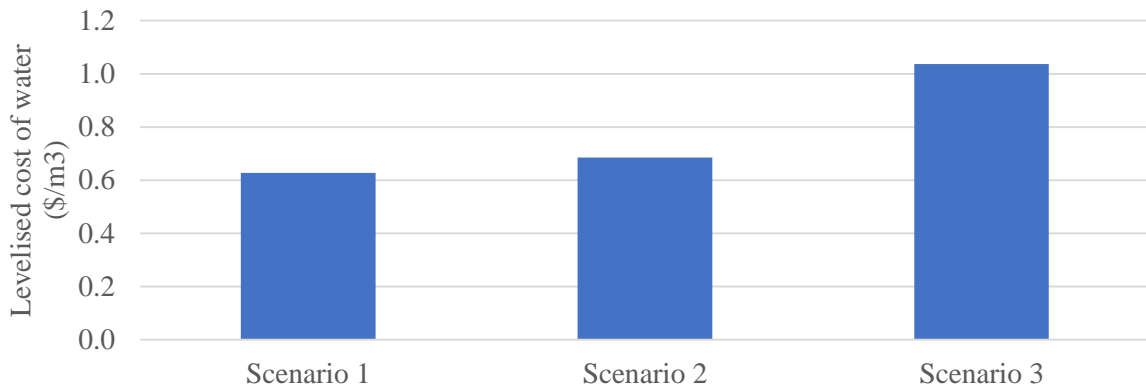


576

577 **Figure 19.** Comparison of LCOE among scenarios

578 **Figure 20** depicts the LCOW for the RO system powered by the power systems with the different  
 579 configurations considered. It can be seen that the PV-RO system without a battery backup system  
 580 has the lowest LCOW of \$ 0.627/m<sup>3</sup>, called Scenario 1. The other scenarios have a slightly higher  
 581 value of \$ 0.686/ m<sup>3</sup> and \$ 1.036/ m<sup>3</sup>, respectively, for Scenario 2 and Scenario 3. The higher LCOW  
 582 means the higher cost to produce the amount of water. The price of the produced water or LCOW  
 583 was then \$ 0.627/m<sup>3</sup>, which is low enough to compete with RO powered by fossil fuels, which range  
 584 between \$ 1 – 2.2/m<sup>3</sup> [18].

585 This study's results show that a non-battery PV-RO desalination system is more feasible than a  
 586 battery and diesel-assisted system. The least NPV indicates this conclusion among the three scenarios  
 587 and the highest cumulative cash flow and IRR value with the shortest payback period. The lowest  
 588 value of LCOE and LCOW shows the low cost of generating energy, following a higher profit range  
 589 from the water sell price.



590

591

**Figure 20.** Comparison of LCOW among scenarios

592

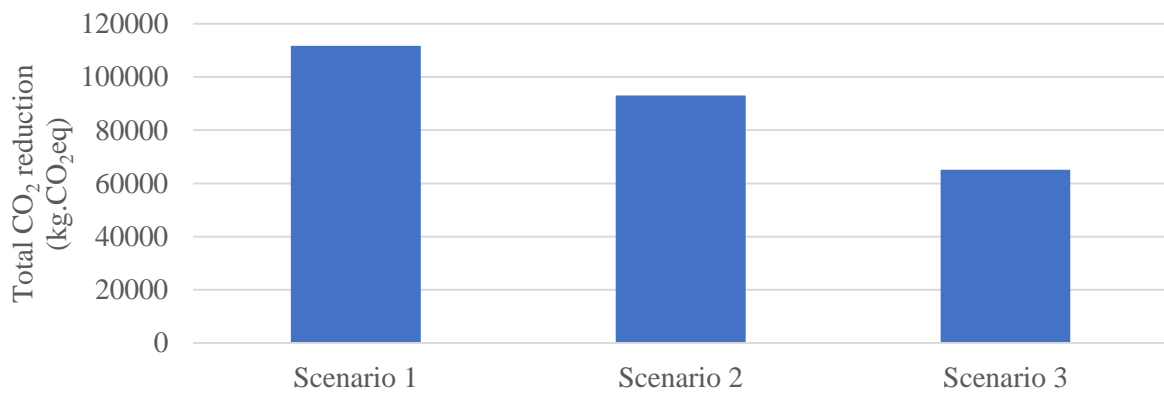
**Figure 21** shows the CO<sub>2</sub> emission avoidance from project scenarios after multiplying the energy generation with the respective emission factor. **Figure 21** also reveals a noticeable difference in a PV-RO system's optimal CO<sub>2</sub> emission reduction compared to a diesel-assisted PV-RO system. As can be seen from **Figure 21**, the CO<sub>2</sub> emission has been reduced up to 45,000 kg.CO<sub>2</sub>eq. from Scenario 1 to Scenario 3.

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**Figure 21.** Comparison of CO<sub>2</sub> emission reduction among scenarios

599

PV-RO system without a battery backup system produces the highest amount of energy generation along with the project so that it can save a considerable amount of CO<sub>2</sub> emission of 111,690 kg.CO<sub>2</sub>eq, while the presence of diesel generation that emits CO<sub>2</sub> has the lowest CO<sub>2</sub> reduction of 65,152.5 kg.CO<sub>2</sub>eq. It can be seen that the integrated renewable energy systems prevent the overproduction of CO<sub>2</sub> emissions and thus reduce overreliance on conventional fossil fuel power

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602

603

604 generation. This result is in accordance with the government's policy to reduce dependence on fossil  
605 fuels while increasing the energy mix in renewable energy for power generation.

#### 606 **4. Conclusion**

607 The Karimunjawa Islands in Indonesia are expected to experience water challenges in the future.  
608 Water desalination technologies are proposed to solve this problem. Subsequently, RO desalination,  
609 which has emerged as a leading and low-cost process, is recommended. However, the desalination  
610 process is energy-intensive and requires significant energy to operate the system. On the other hand,  
611 the PV technology that converts solar energy to electricity is a prospective power source for the  
612 desalination system. The abundant solar potential is proposed to provide this RO desalination plant  
613 power.

614 This study has systematically analyzed several PV-RO desalination systems with a 5 m<sup>3</sup>/day capacity  
615 for daily use on Parang Islands. Three different scenarios are studied: batteryless, battery, and diesel  
616 generator assisted. The analysis results show that the batteryless PV-RO system (scenario 1) is the  
617 most optimized and economically feasible among other strategies. Scenario 1 comprises 6.3 kW PV  
618 panels installed with a 2-day water storage tank during prolonged periods with less sunshine. The  
619 LCOE of scenario 1 was found to be \$ 0.154/kWh, with the LCOW calculated to be \$ 0.627/m<sup>3</sup>. The  
620 NPV and payback period of the optimized system was \$ 21,143.13 and 5 years, respectively. The  
621 analysis indicated the PV-RO system is economically feasible for the site.

622 Harnessing renewable resources for power generation decreases fossil fuel consumption and avoids  
623 harmful emissions. For this reason, the diesel-assisted PV-RO system (scenario 3) is the less  
624 preferable option because of its high pollutant emissions. The CO<sub>2</sub> emissions avoidance by this  
625 system was 65,152.5 kg.CO<sub>2</sub>eq, while the optimized system could eliminate 111,690 kg.CO<sub>2</sub>eq per  
626 year. Thus, it was found that using a diesel generator could increase the annual CO<sub>2</sub> emissions by  
627 50%.

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## 633 **Declaration of Competing Interest**

634 The authors declare that they have no known competing financial interests or personal relationships  
635 that could have appeared to influence the work reported in this paper.

## 636 **Data availability**

637 Data will be made available on request.

## 638 **Author contributions**

639 **Athaya Fairuz:** Conceptualization, Methodology, Data curation and Writing- Original draft  
640 preparation. **M.F. Umam:** Formal analysis, Writing- Original draft preparation. **M. Hasanuzzaman:**  
641 Conceptualization, Writing- Reviewing and Editing, Funding acquisition, and Supervision. **NA.**  
642 **Rahim:** Writing- Reviewing and Editing, Funding acquisition, and Supervision. **IM Mujtaba:**  
643 Conceptualization, Writing- Reviewing and Editing.

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